



RF Heat Load Compensation for the European XFEL

J. Penning

with

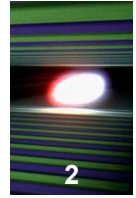
M. Clausen, B. Schoeneburg, O. Korth

and additional material from

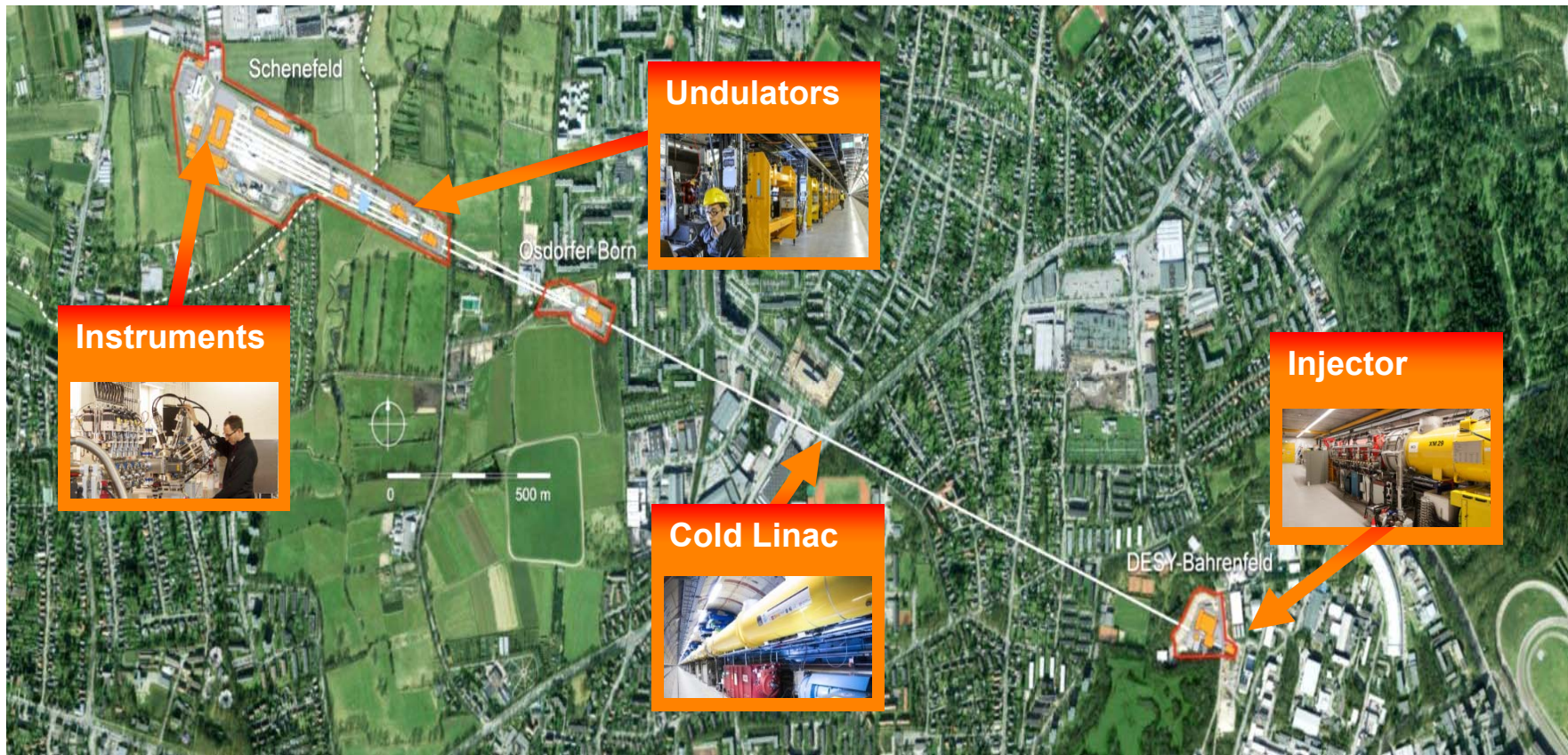
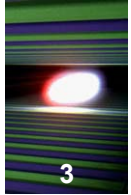
J. Eschke, T. Schnautz, M. Omet, J. Branlard

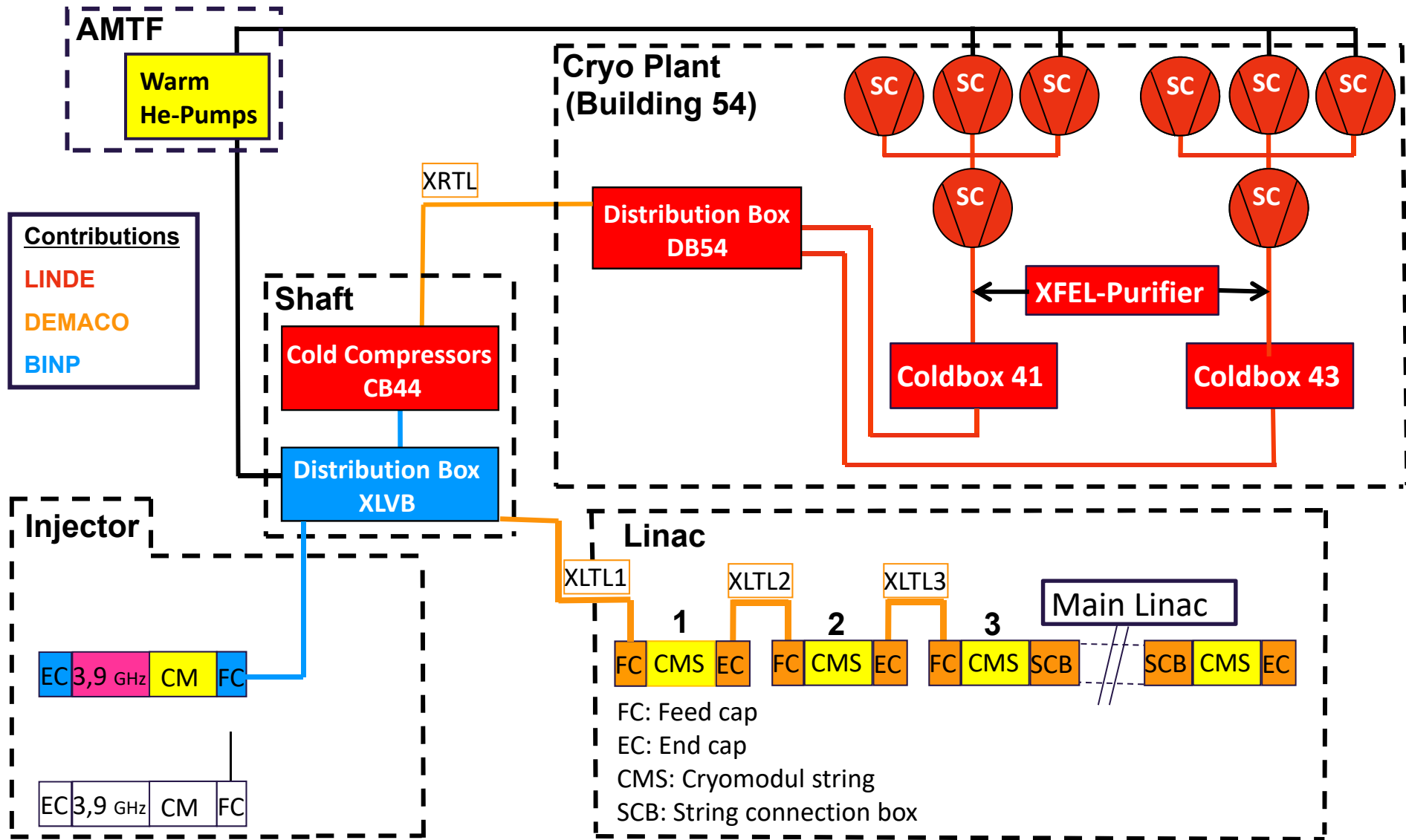
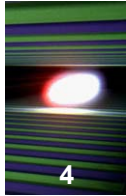
Deutsches Elektronen-Synchrotron (DESY), Hamburg, Germany



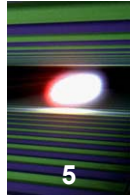


- **The XFEL: Drilling down to our topic**
- Cold compressors: Powerful but sensitive
- Automatic Heat Load Compensation (AHLC)
 - How to compensate
 - How to calculate
 - Limitations of current approach
 - Implementation
 - Robustness issues
 - Summary

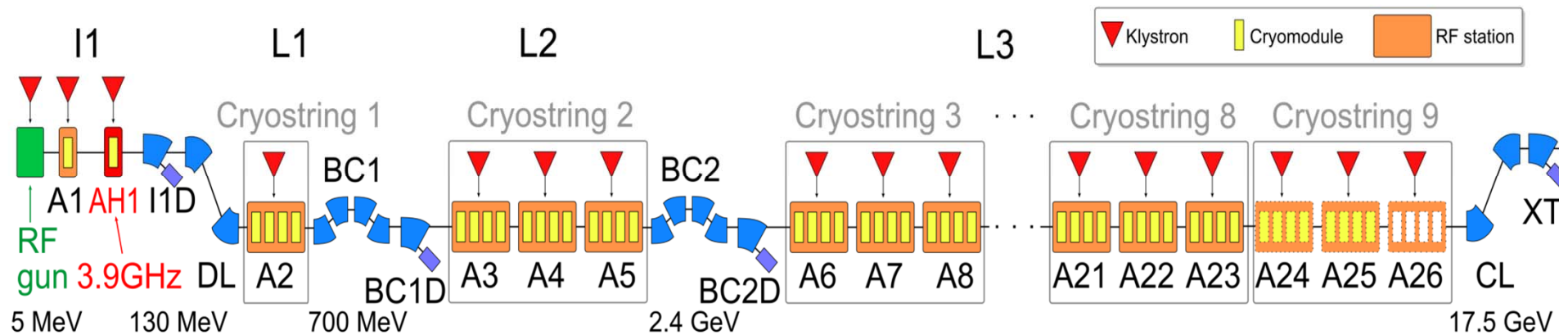


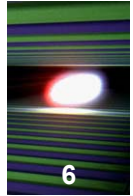


Focusing on the cryo installation



- Injector and 3 Linacs
- 9 Cryo-Strings
- 96 Cryo-Modules
- ~800 Cavities
- 32 cavities per RF station
- Design energy 17.5 GeV

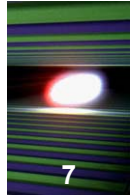




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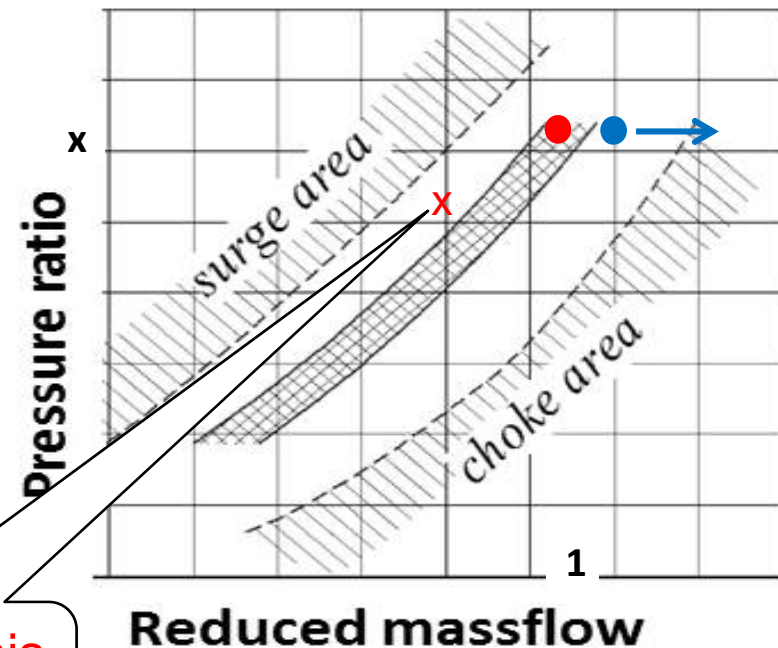
Cold compressors

General challenges (repeated)



- Cold compressors are turbomachines and hence very sensitive towards massflow-, temperature- and pressure- changes in the 2K-return flow (but the **massflow-stability** is most important)
- Choke operation: Should be avoided as cryo capacity decreases
- Surge operation: Not possible - breakdown of operation

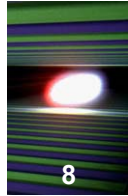
Coldboxes also want stable flow



What about this working point?

Cold compressors

Operational experiences – 2K pressure stability (repeated)

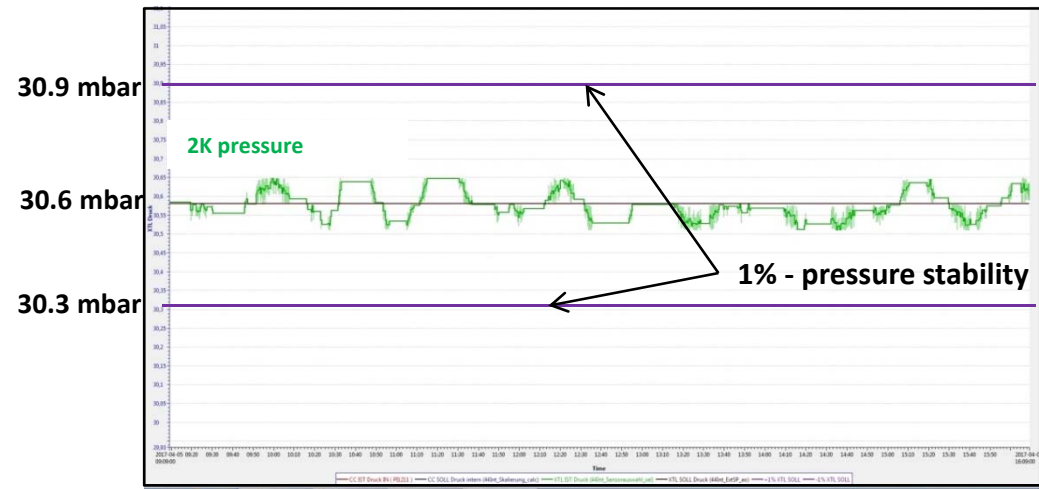


Cold compressors: 2K Pressure stability

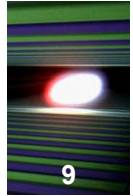
- Specified pressure stability: 1% (31 mbar +/- 0.3 mbar)
- Cascaded regulation for pressure adjustment in 2K circuit is used (DESY)
- **Automatic heat load compensation (DESY): Changes in the 2K return flow - caused by dynamic RF operation - are determined automatically and compensation takes place in the linac by automatic heating in the 2K liquid helium**

Conclusion:

- Cold compressors deliver a pressure stability better than 0.3%, which is much better than internally specified.
- Heat load changes –caused by dyn. RF operation- can be compensated perfectly well by AHLC



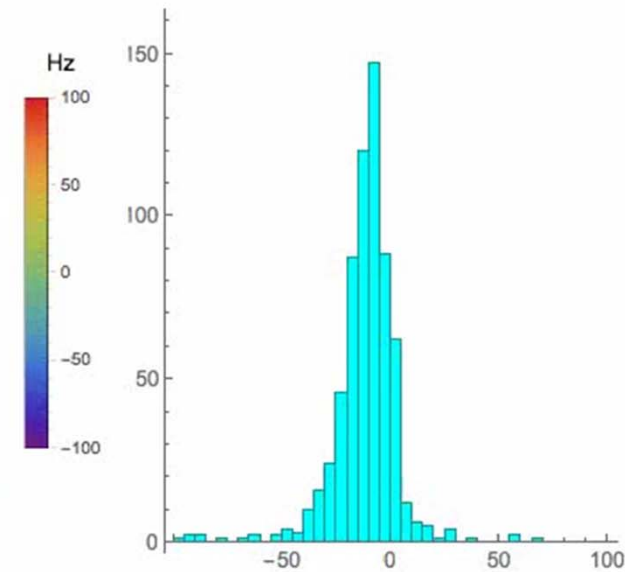
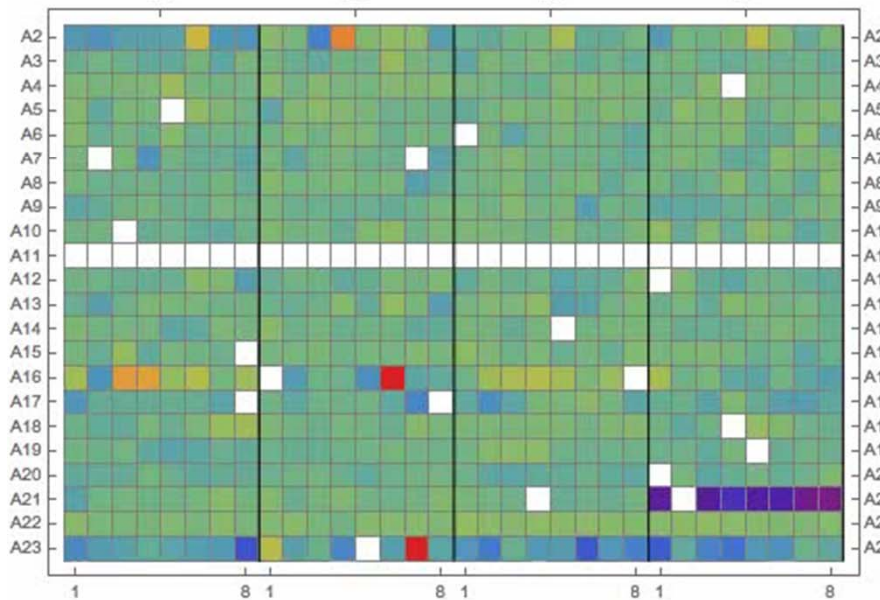
Excursion: Importance of pressure stability



- Cavity Detuning vs. He-Pressure
- Study by Julien Branlard
- Will be presented in September at Linear Accelerator Conference



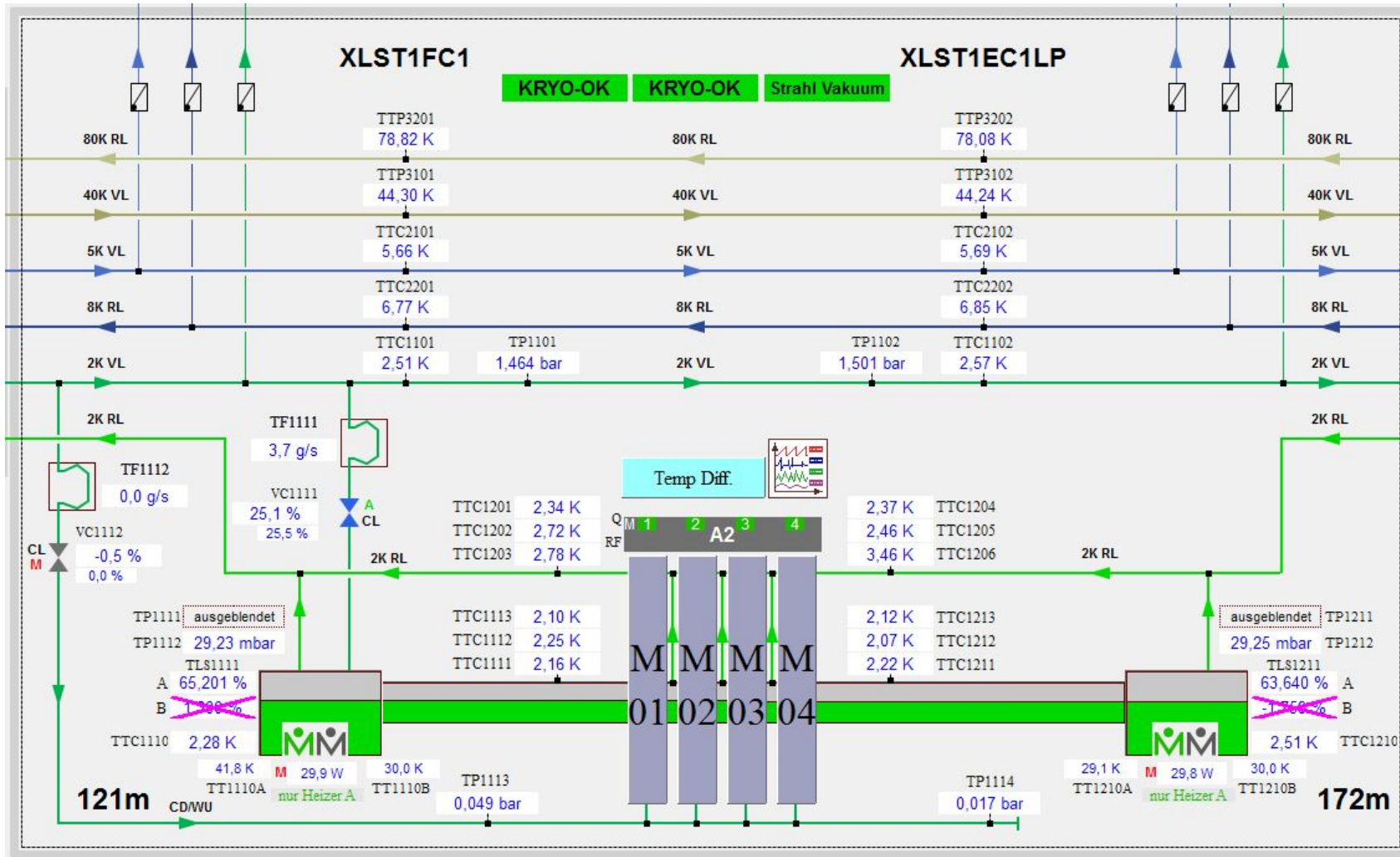
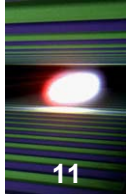
Average -10.0 Hz



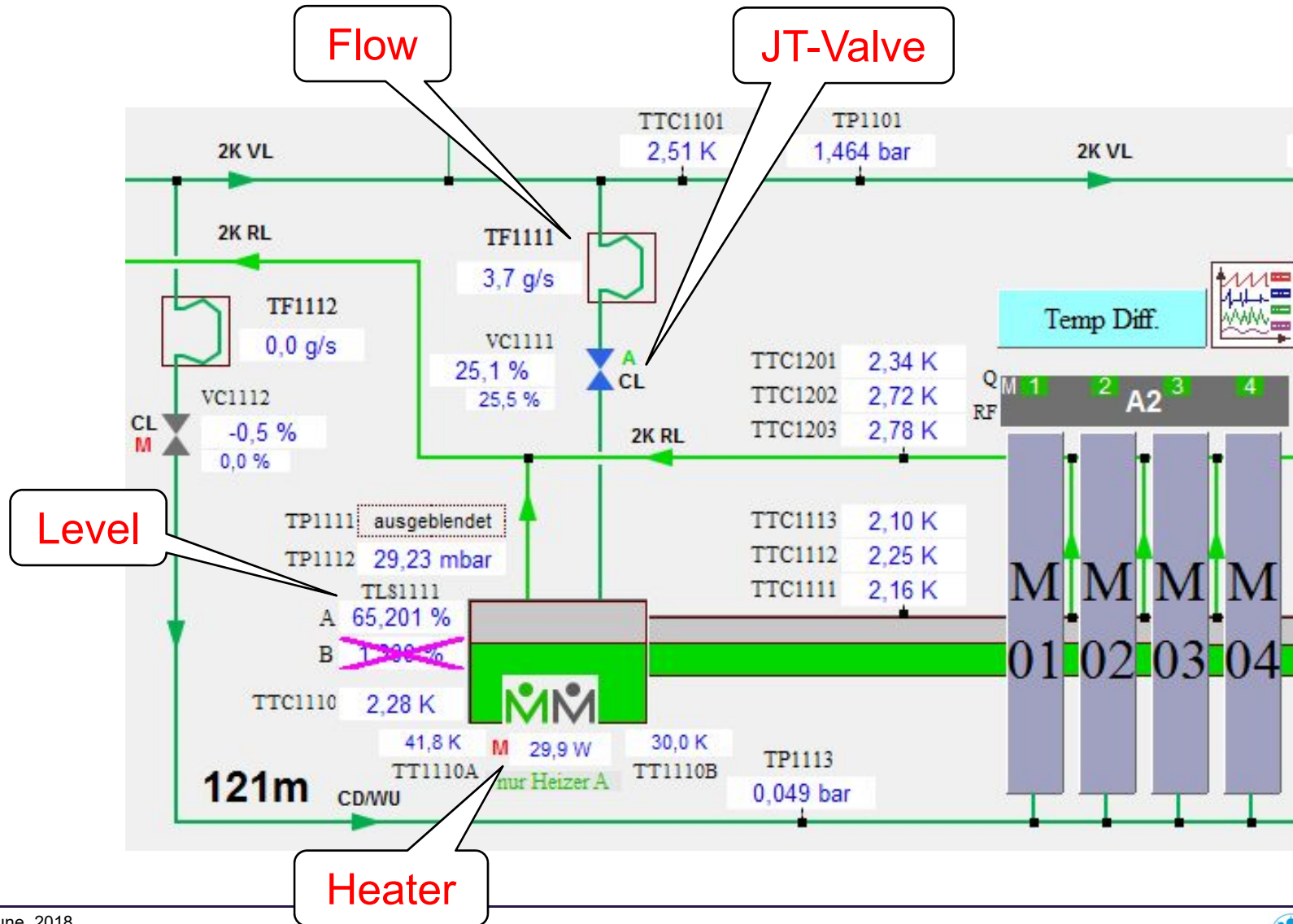
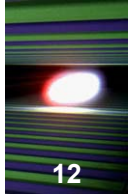


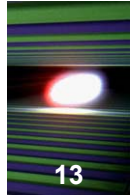
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Flowdiagram of Linac 1



Sensors and Actuators





- During Cooldown
 - the JT-Valve was controlled by the flow sensor
 - the main concern was stable operation of the coldboxes
- During stable operation
 - the JT-Valve is controlled by the **level sensor**.
 - the main concern now is the level of the He-bath for the cavities and the magnets.



- The Heaters allow for a steady power dissipation which can be **reduced** when the RF is applied to the cavities.
- The Heaters are set to **some value** which is higher than the expected power introduced by RF.
- **Some value** is based on experience from the cavity tests and fine tuned by the operators.
- The **reduction** of the Heater power is calculated automatically from RF operational data.

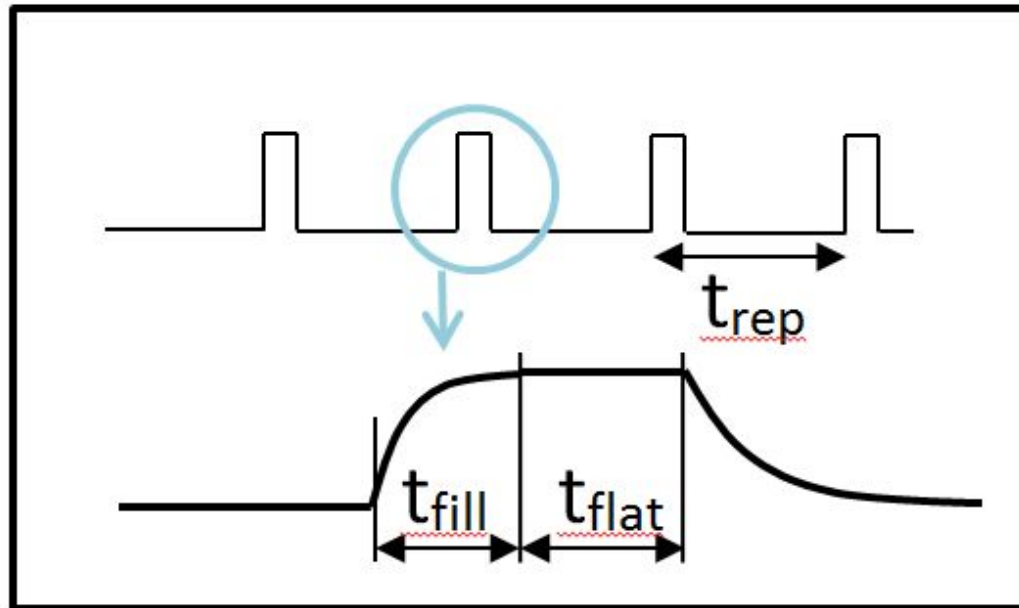
AHLC comes
into play



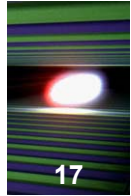
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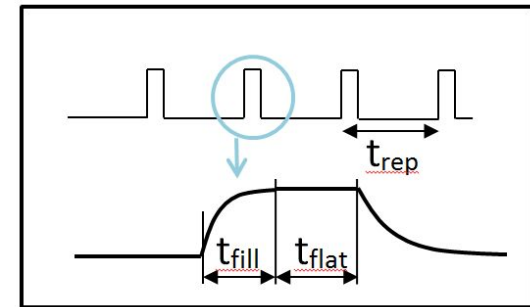
- RF pulses have a certain repetition rate
- Each pulse has a structure
 - Filling until a certain power is reached
 - Stay flat at that power
 - Switch off and let decrease



Detailed calculation: Filling



- Filling is achieved with a constant voltage, it is clipped when the desired power has been reached.
- The Energy introduced to the cavity is



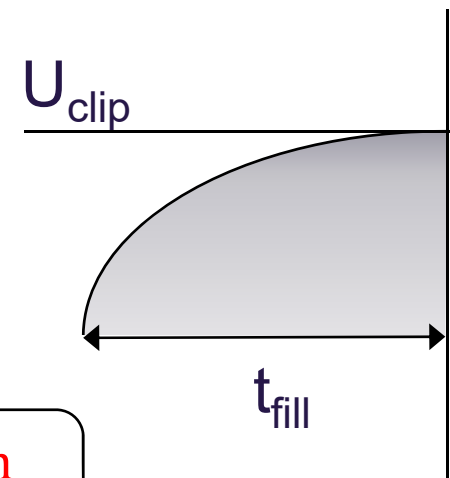
$$E_{fill} = \int_0^{t_{fill}} P(t) dt \quad \text{with}$$

$$P(t) \sim U(t)^2 \quad \text{and}$$

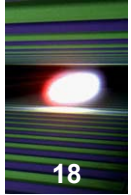
$$U(t) \sim U * (1 - e^{-\lambda t})$$

- Solving yields

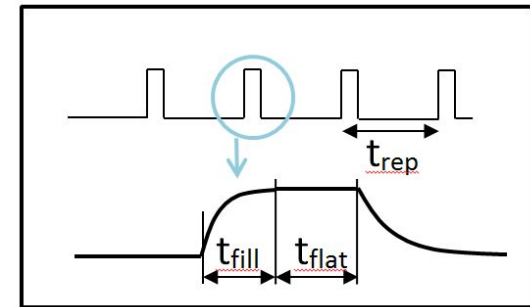
$$E_{fill} = P_{forw} * t_{fill} * 0.38$$



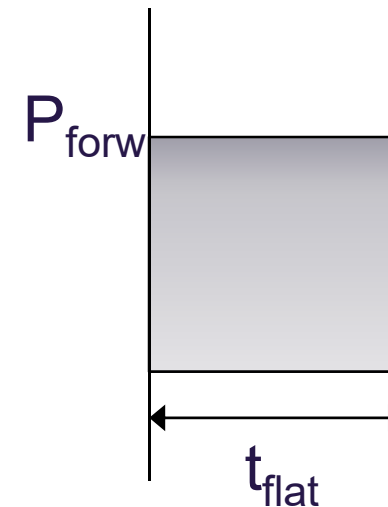
λ is known from the tests



- During the flat top the voltage is kept at the clipped level.
- The dissipated energy is only dependent on the time and the forward power applied.

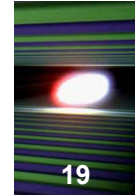


$$E_{\text{flat}} = P_{\text{forw}} * t_{\text{flat}}$$



Detailed calculation: Decrease

λ is known from the tests

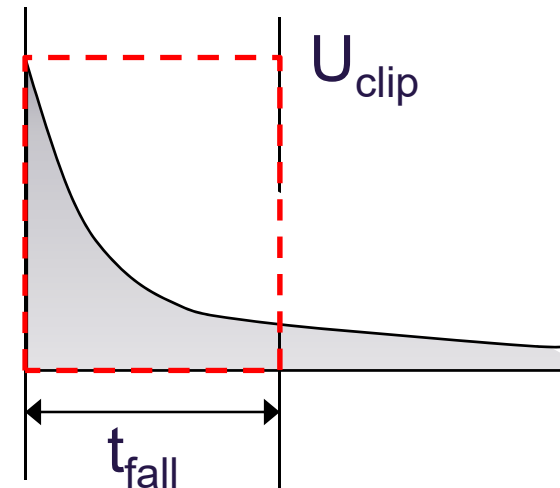
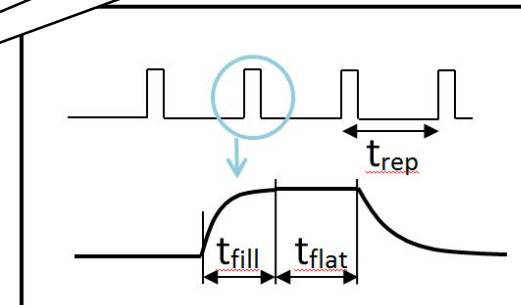


- After switching off, the voltage decreases.
- The energy introduced to the cavity is $E_{\text{fall}} \sim \int_0^{\infty} U^2 * e^{-\lambda t} dt$
- This is equal to a square of fixed length (t_{fall}) by forward power.

- Solving yields

$$E_{\text{fall}} = P_{\text{forw}} * t_{\text{fall}}$$

t_{fall} being constant ($\sim 500 \mu\text{s}$)



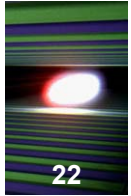


$$P_{\text{diss}} \sim (E_{\text{fill}} + E_{\text{flat}} + E_{\text{fall}}) * f_{\text{rep}} * \text{Usage}$$
$$= K * P_{\text{forw}} * (t_{\text{fill}} * 0.38 + t_{\text{flat}} + t_{\text{fall}}) * f_{\text{rep}} * \text{Usage}$$

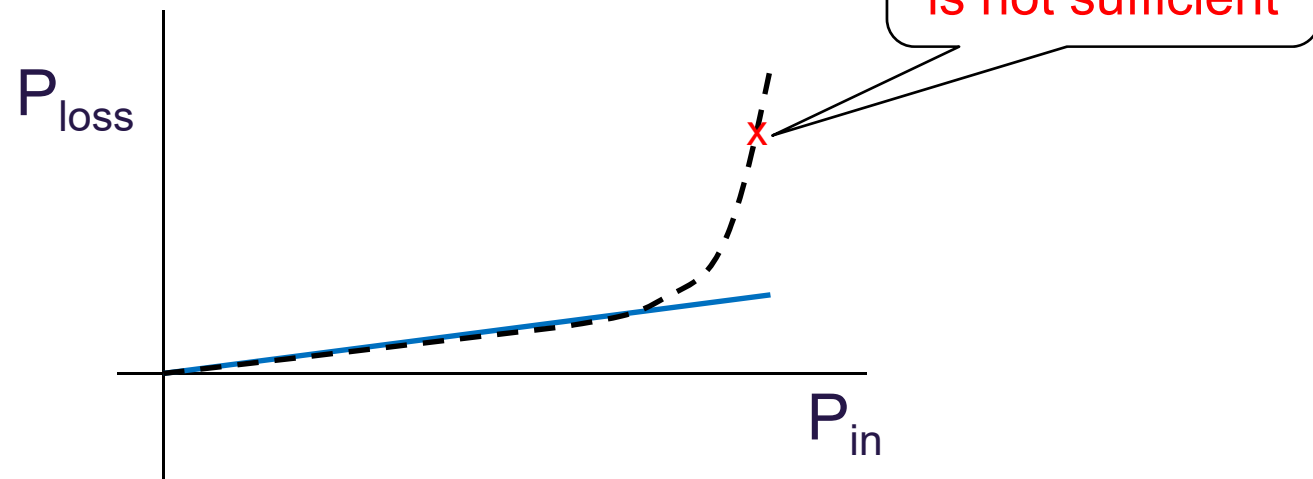
- ***K*** is an empiric factor of about $4 * 10^{-7}$
Pre-calculated from cavity tests
Refined after operating experience
- ***P_{forw}*** is the power as measured by the RF station
which is distributed to 32 cavities each.
- ***f_{rep}*** is the repetition rate
- ***Usage*** Only active cavities are taken into account



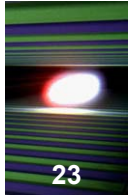
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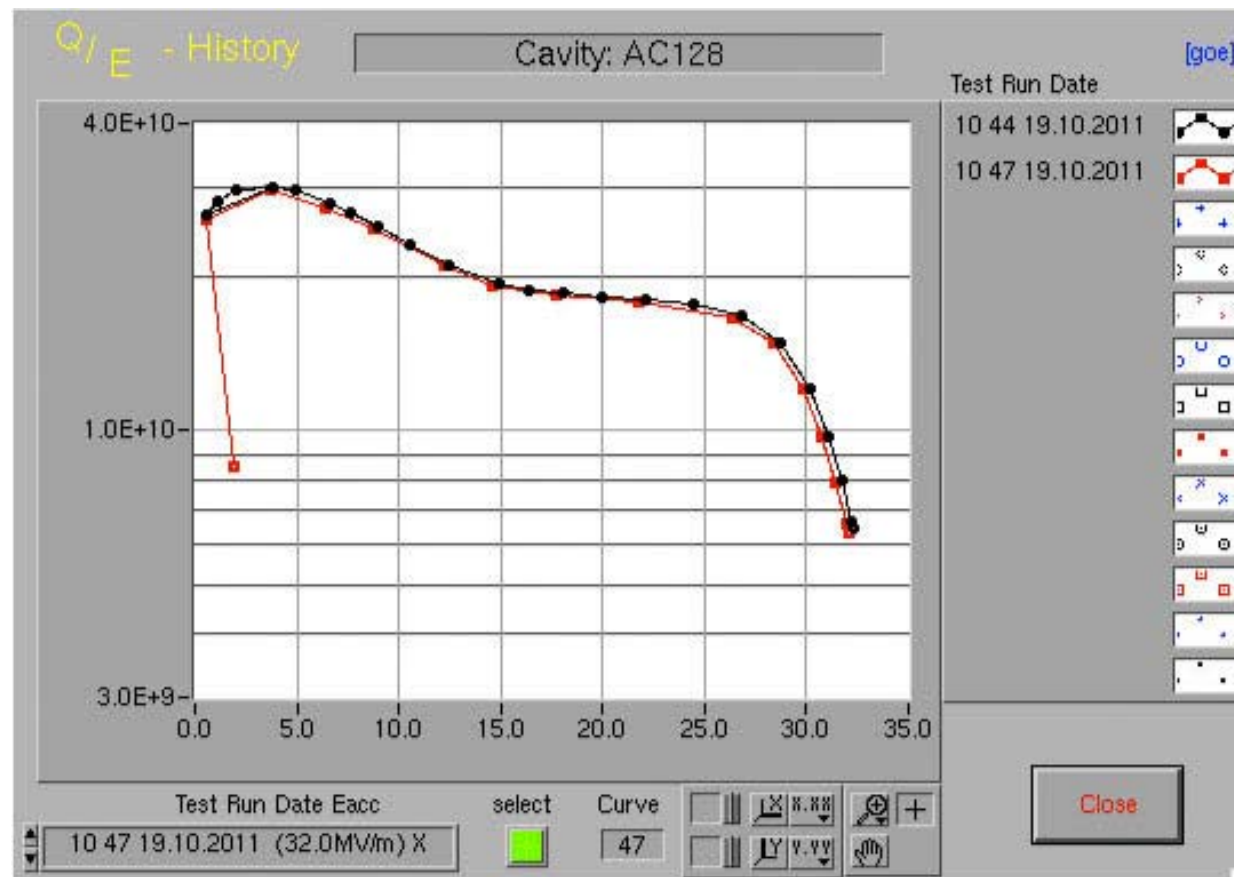
- Simple approach
 - Linear compensation only
 - Treat all cavities the same

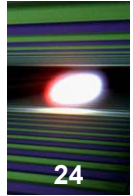


$$P_{\text{diss}} = K * P_{\text{forw}} * (t_{\text{fill}} * 0.38 + t_{\text{flat}} + t_{\text{fall}}) * f_{\text{rep}} * \text{Usage}$$

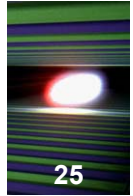


- Quality vs. Energy shows non-linear behaviour

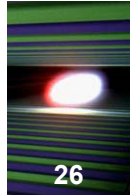




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- Try the most simple thing first
- Be able to modify the crucial part while maintaining operation
 - AHLC runs outside the process controller of the linac
 - Software updates to AHLC during normal operation of the linac are possible
 - AHLC could be enhanced significantly without overloading the process controller of the linac



- Rate-of-change (1W/s) helps survive
 - intermittent communication breakdowns
 - calculation errors
- Careful selection of manual setpoint for the heaters
 - Keep JT-valves always a bit open
 - Keep heaters always a bit on
 - That ensures a bit of control range always



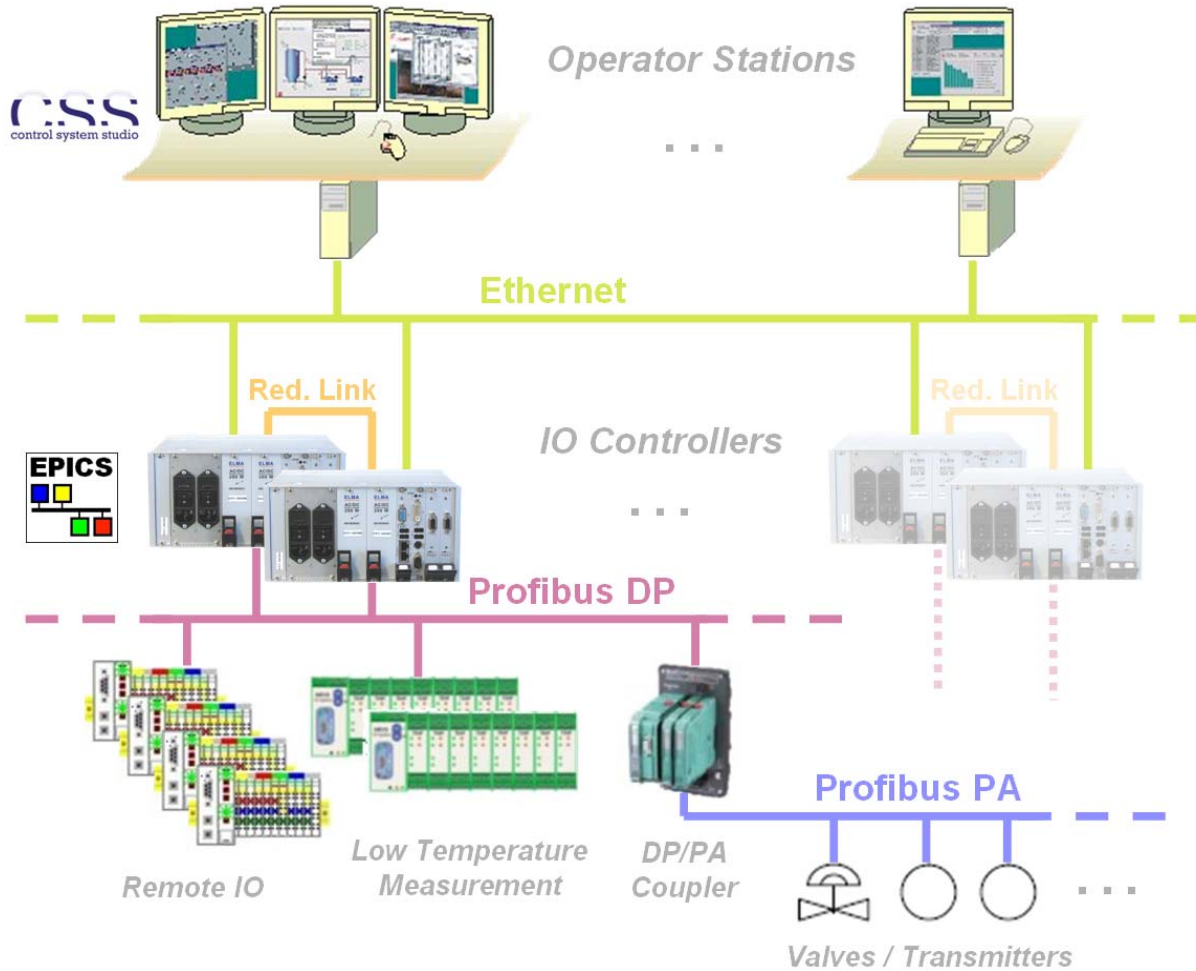
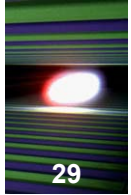
- What happens when cavities are driven in the non-linear range?
 - AHLC cannot handle this
 - Usually happens on announcement from RF group
 - Maximum Gradient Task Force tries to push the limits
 - One RF station at a time
 - Supported by an operator

Quenches
switch off RF



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Architecture of Control System



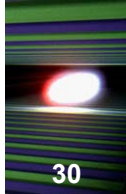
■ Operators Workplace

■ IP-Network

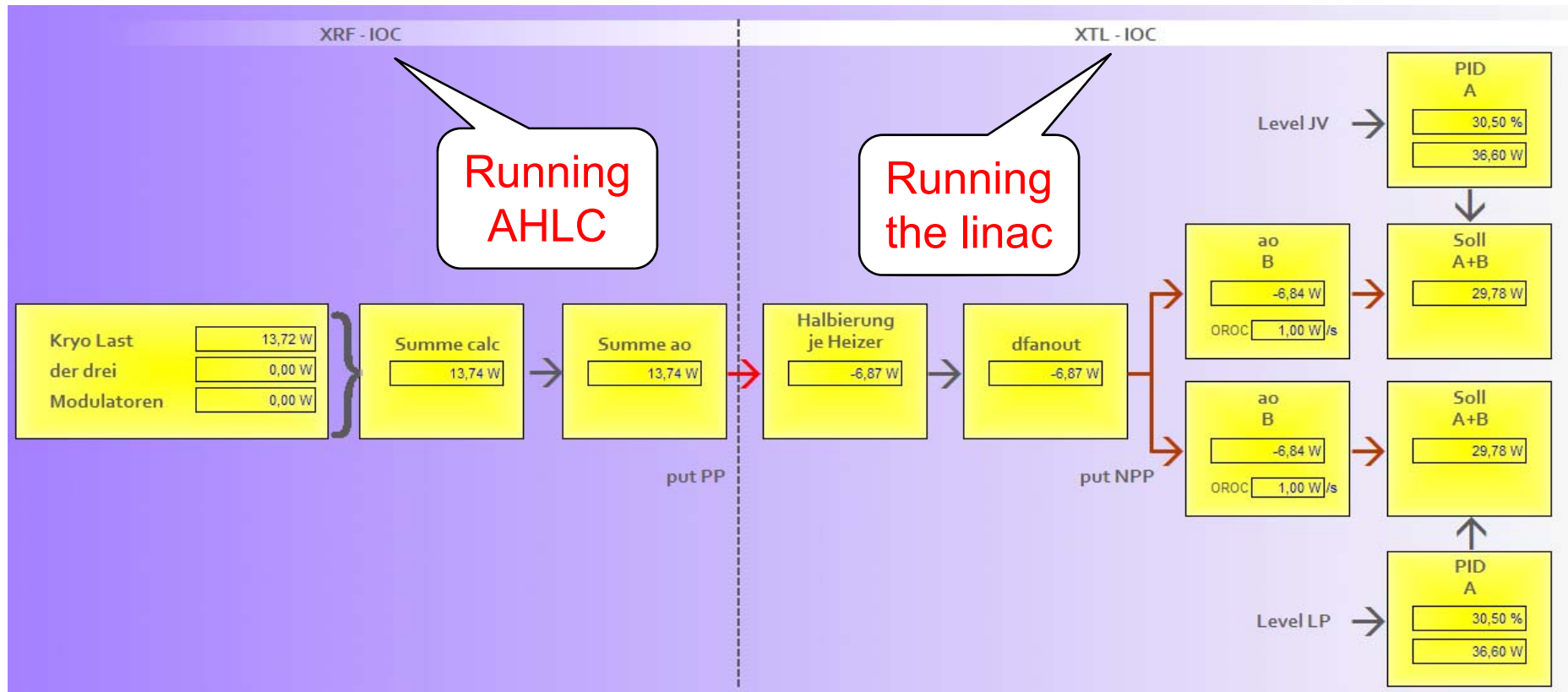
■ Process Control Hardware

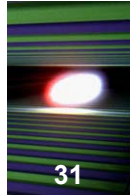
■ Fieldbus-Network

■ Sensors / Actuators

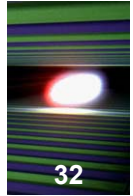


- Make use of two process controllers (IOCs)

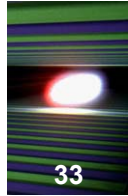




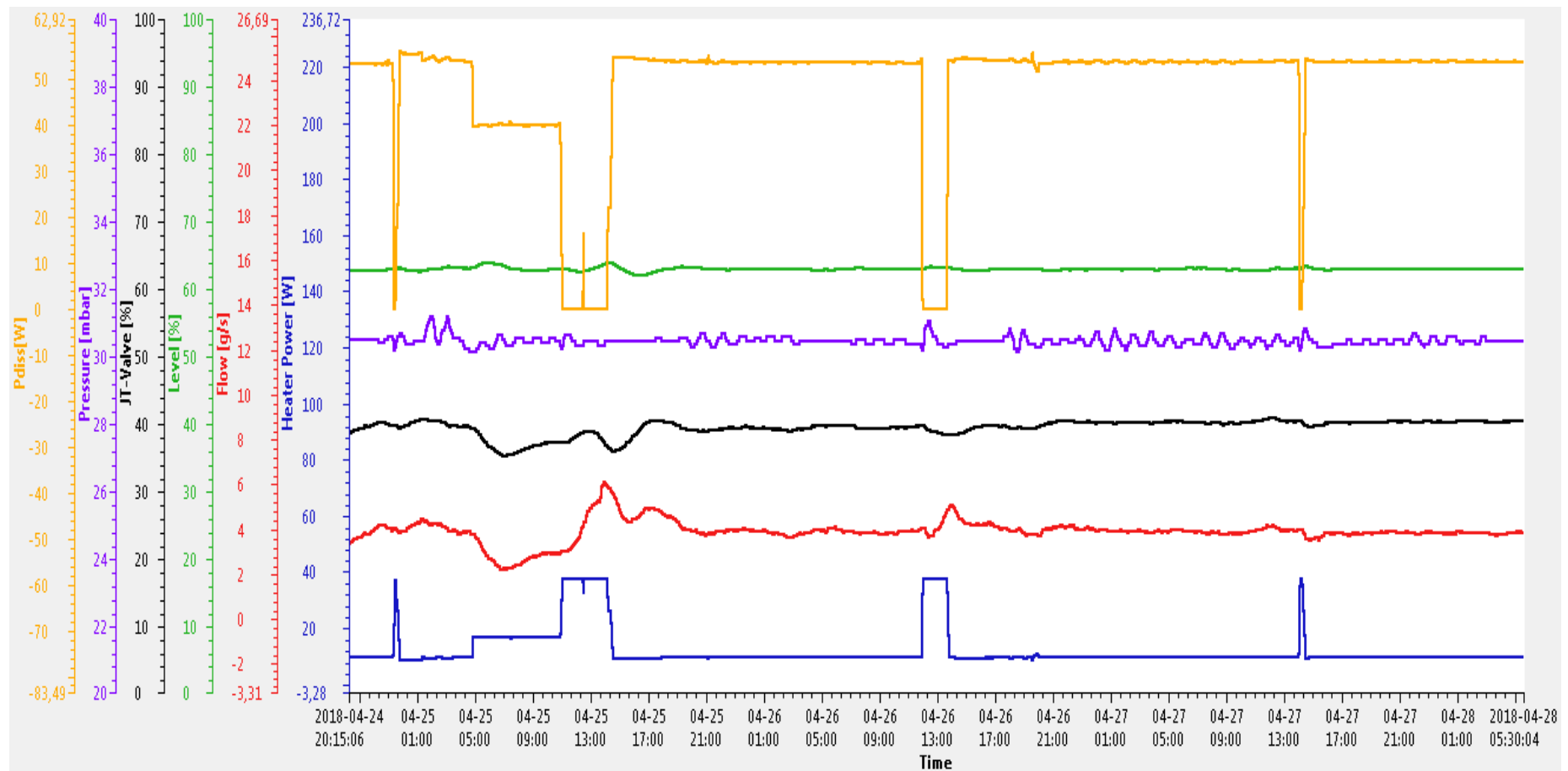
- What happens if RF data cannot be retrieved?
 - Communication channels announce alarms so operators will notice
 - Current values freeze
- What happens if AHLC-process controller stops or is updated?
 - There will be no more updates via the process border
 - So the current values will be kept in the linacs process controller
 - The operator will be noticed because the AHLC-process controller failed

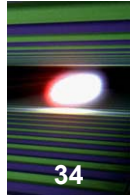


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- From top: RF power, Level, He-Pressure, JT-Valve Readback, Flow, Heater Readback

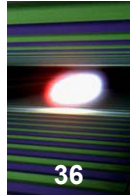




- If MGTF recommends operation near the non-linear range
 - We will make an approximation
 - The first step might take individual cavities into account
 - We can update AHLC any time



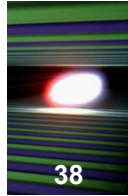
- AHLC tries to keep the flow of each cryo string stable
 - It calculates the heat introduced by RF operation from RF live data
 - By reducing the (manually preset) heater power the dissipated heat stays the same
 - Currently only the linear losses can be compensated, near quenching the compensation falls short
 - For ease of implementation all cavities are treated the same
 - The implementation handles communication breakdown and allows for live updates



Thank you for your attention



Additional slides



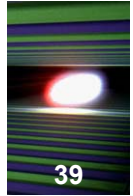
Cryogenic plant-capacity: Performance requirements vs. performance results:

1. **Parallel coldbox** operation: CB41 and CB43 with cold compressors (CB44)
2. Single coldbox operation: CB41 or CB43 with cold compressors (CB44)

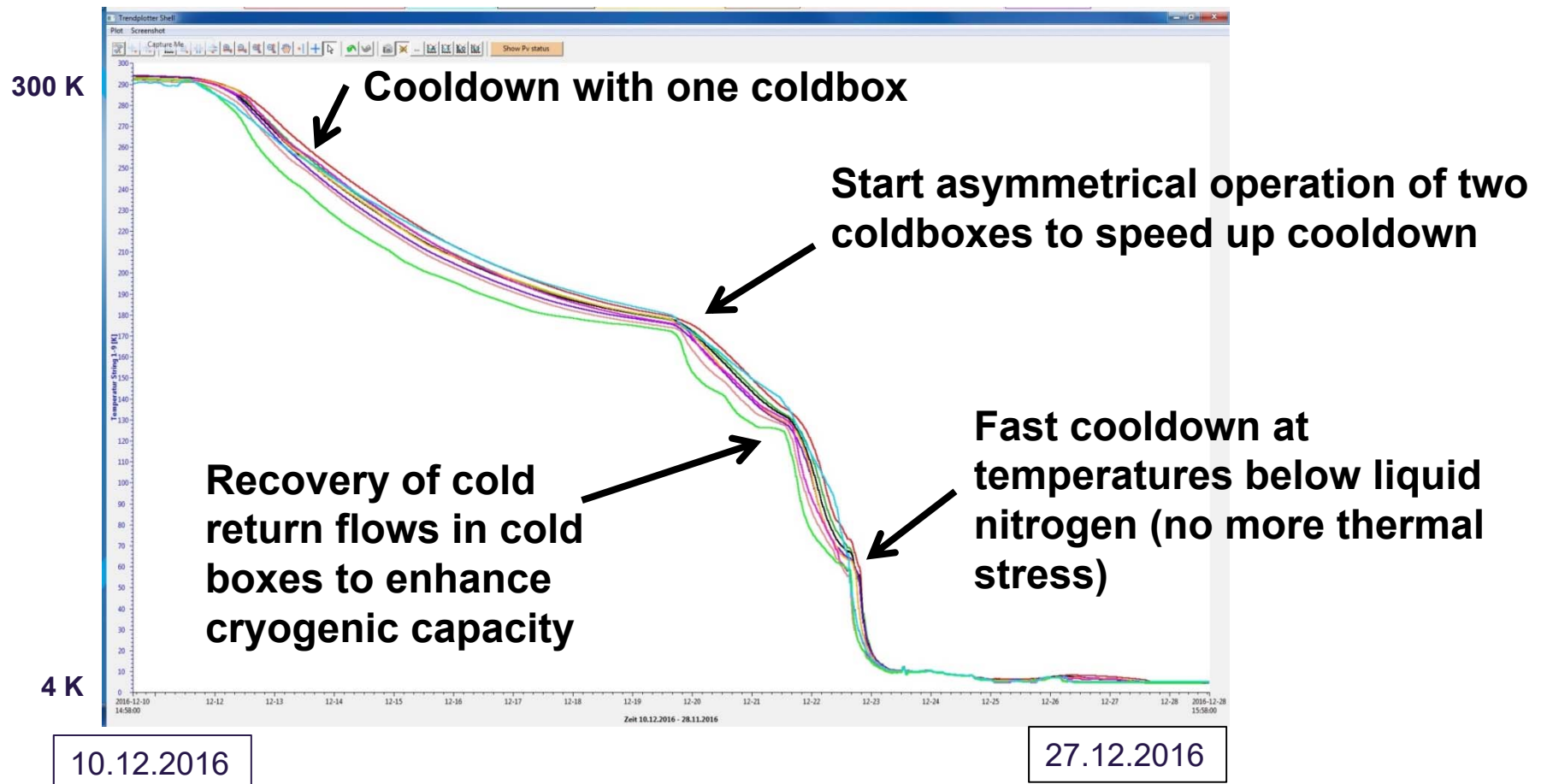
Cooling loop	unit	DESY calculated	DESY specification (calculated + safety margin)	Linde offer (guaranteed)	Linde offer (expected)	Test results CB 41 & CB 43
2K	kW	1.46	1.9	1.9	2.01	> 1.9
5K – 8K	kW	2.4	3.6	3.6	3.95	4.0
40K – 80K	kW	16.0	24	24	26.12	25.9

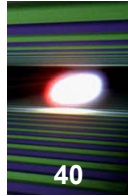
Conclusion:

- **Guarantee values for parallel coldbox operation have been exceeded!**



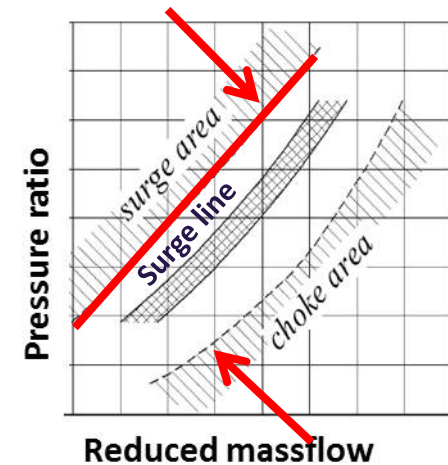
First cooldown: XFEL Linac

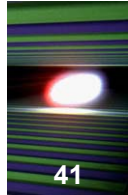




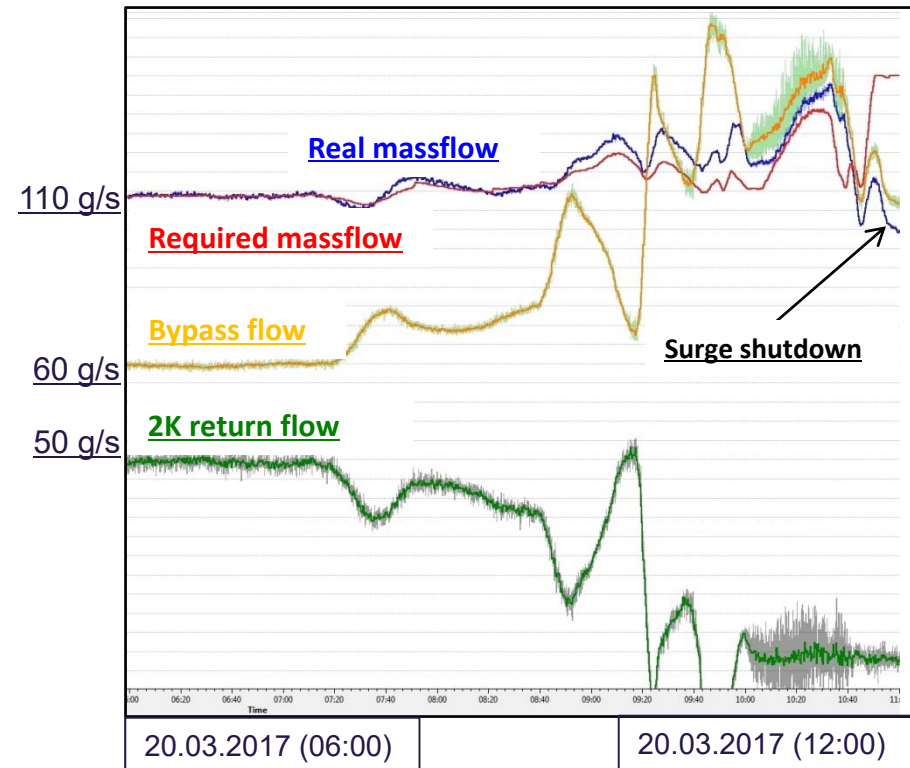
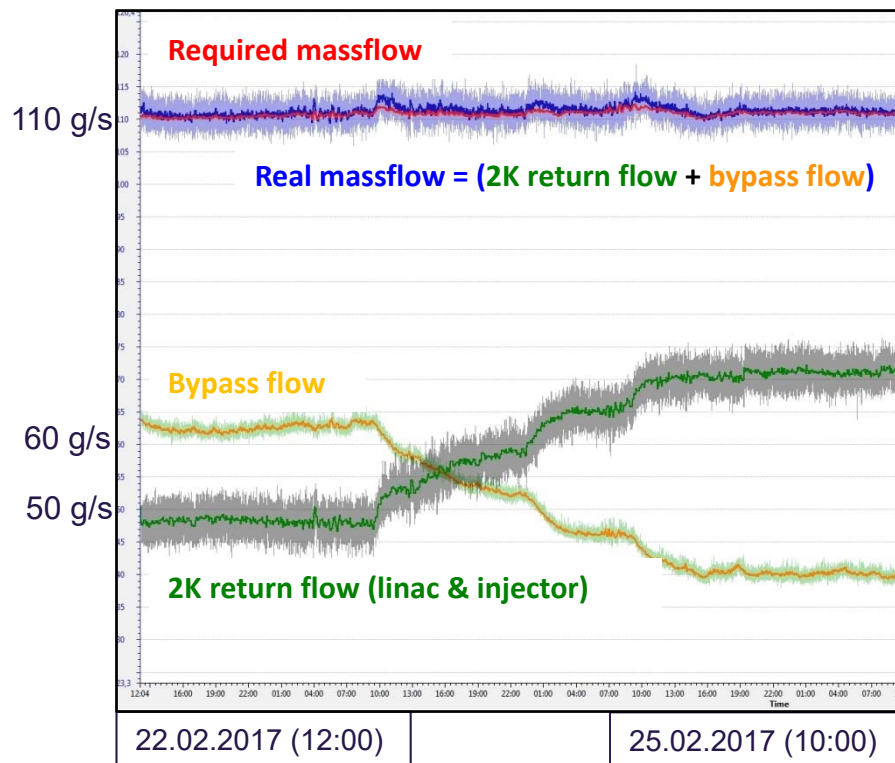
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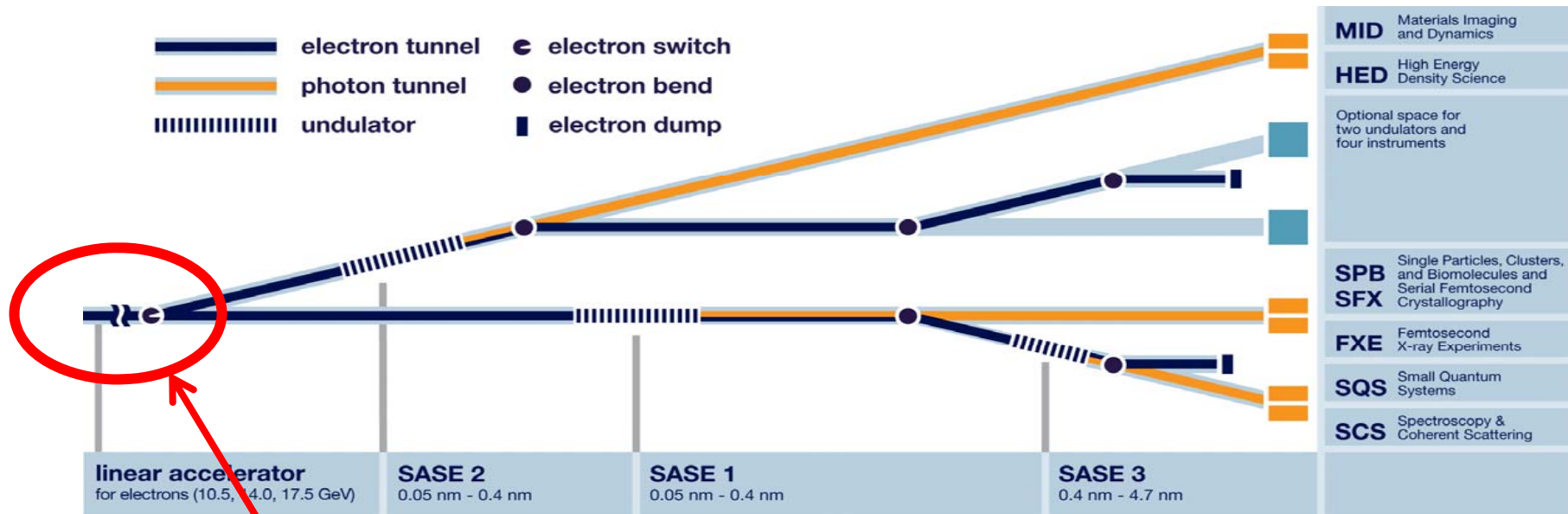
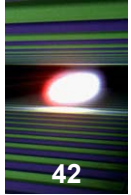


Bypass operation: Massflow compensation



Conclusion:

- CC-bypass operation delivers reasonable reactions on changes in 2K return flow



Focusing on the cold linac

XFEL:

- Length of accelerator: 1500m
- Length of facility: 3400m
- Accelerator modules : 96
- Max. electron energy: 17.5 GeV
- Start of regular operation: July 1st,2017